Lecture 23: Resonance Phenomena

Reading:

Kreyszig Sections: 2.8, 2.9, 3.1, 3.2, 3.3 (pages84–90, 91–96, 105–111, 111–115, 116–121)

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Resonance Phenomena

There is a set of alternative solutions to damped-forced near-resonance behavior at http://pruffle.mit.edu/3.016-2008/mathematica-

The physics of an isolated damped linear harmonic oscillator follows from the behavior of the homogeneous equation: 14

paradigms.html that are designed to be instructive.

 $M\frac{d^2y(t)}{dt^2} + \eta l_o \frac{dy(t)}{dt} + K_s y(t) = 0$

(23-1)

This equation is the sum of three forces:

inertial force depending on the acceleration of the object.

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drag force depending on the velocity of the object.

spring force depends on the displacement of the object.

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The system is autonomous in the sense that everything depends on the system itself; there are no outside agents changing the system.

¹⁴ A concise and descriptive description of fairly general harmonic oscillator behavior appears at http://hypertextbook.com/chaos/41.shtml

The zero on the right-hand-side of Eq. 23-1 implies that there are no external forces applied to the system. The system oscillates with a characteristic frequency $\omega = \sqrt{K_s/M}$ with amplitude that are damped by a characteristic time $\tau = (2M)/(\eta l_o)$ (i.e., the amplitude is damped $\propto \exp(-t/\tau)$.)



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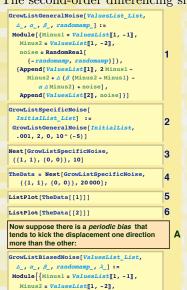
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Simulating Harmonic Oscillation with Biased and Unbiased Noise

The second-order differencing simulation of a harmonic oscillator is modified to include white and biased stochastic nudging.



biasednoise = 0.5 randomamp

GrowListSpecificBiasedNoise[InitialList_List] :=

GrowListBiasedNoise[InitialList, .001, 2, 0, 10^(-6), 4500]

{Append[ValuesList[1]], 2 Minus1 -Minus2 + 4 ((Minus2 - Minus1) -

 $(\cos[(2 \pi \text{Length}[ValuesList[1]])))$ | + RandomReal[{-1, 1}])},

α Δ Minus2) + biasednoise], Append[ValuesList[2], biasednoise]}

- 1: GrowListGeneralNoise is extended from a previous example for simulating $\ddot{y} + \beta \dot{y} + \alpha y = 0$ (GrowList in example 21-1) and adds a random uniform displacement $y + \delta$, $\delta \in (-\text{randomamp}, \text{randomamp})$ at each iteration. The ValuesList_List argument should be a list containing two lists: the first list is comprised of the sequence of displacements y; the second list records the corresponding stochastic displacement δ . The function uses a list's two previous values and Append and to grow the list iteratively.
- 4: Exemplary data from 2×10^5 iterations (using Nest) is produced for the specific case of $\Delta = 0.001$, $\alpha = 2, \beta = 0.$
- 5: The displacements (i.e., first list) are plotted with ListPlot.
- The random 'nudges' (i.e., second list) are also plotted.
- 7: Biased nudges are simulated with GrowListBiasedNoise. This extends the unbiased example above, by including a wavelength for a cosine-biased random amplitude. A sample, δ , from the uniform random distribution as above is selected and then multiplied by $\cos 2\pi t/\lambda$. The time-like variable is simulated with Length and the current data.
- 10: The biased data for approximately the resonance condition for the same model parameters above is plotted with the biased noise.

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A general model for a damped and forced harmonic oscillator is

$$M\frac{d^2y(t)}{dt^2} + \eta l_o \frac{dy(t)}{dt} + K_s y(t) = F_{app}(t)$$

(23-2) 3 016

where F_{app} represents a time-dependent applied force to the mass M.

General Solutions to Non-homogeneous ODEs

Equation 23-2 is a non-homogeneous ODE—the functions and its derivatives appear on one side and an arbitrary function appears on the other. The general solution to Eq. 23-2 will be the sum of two parts:

$$y_{gen}(t) = y_{part}(t) + y_{homog}(t)$$
$$y_{gen}(t) = y_{F_{app}}(t) + y_{homog}(t)$$

$$y_{homg}(t) = \begin{cases} C_{+}e^{-|\lambda+|t} + C_{-}e^{-|\lambda-|t} & (\eta l_{o})^{2} > 4MK_{s} & \text{Over-damped} \\ C_{1}e^{-|\lambda|t} + C_{2}te^{-|\lambda|t} & (\eta l_{o})^{2} = 4MK_{s} & \text{Critical Damping} \\ C_{+}e^{-|\text{Re}\lambda|t}e^{\imath|\text{Im}\lambda|t} + C_{-}e^{-|\text{Re}\lambda|t}e^{-\imath|\text{Im}\lambda|t} & (\eta l_{o})^{2} < 4MK_{s} & \text{Under-damped} \end{cases}$$

$$(23-4)$$

where $y_{part} \equiv y_{F_{app}}$ is the solution for the particular F_{app} on the right-hand-side and y_{homog} is the solution for the right-hand-side being zero. Adding the homogeneous solution y_{homog} to the particular solution y_{part} is equivalent to adding a "zero" to the applied force F_{app}

Interesting cases arise when the applied force is periodic $F_{app}(t) = F_{app}(t+T) = F_{app}(t+2\pi/\omega_{app})$, especially when the applied frequency, ω_{app} is close to the the characteristic frequency of the oscillator $\omega_{char} = \sqrt{K_s/M}$.

Modal Analysis

For the case of a periodic forcing function, the time-dependent force can be represented by a Fourier Series. Because the second-order ODE (Eq. 23-2) is linear, the particular solutions for each term in a Fourier series can be summed. Therefore,

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particular solutions can be analyzed for one trigonometric term at a time:

$$M\frac{d^2y(t)}{dt^2} + \eta l_o \frac{dy(t)}{dt} + K_s y(t) = F_{app} \cos(\omega_{app} t)$$

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There are three general cases for the particular solution:

	Condition	Solution for $F(t) = F_{app} \cos(\omega_{app} t)$
Undamped, Frequency- Mismatch	$\eta = 0$ $\omega_{char}^2 = \frac{K_s}{M} \neq \omega_{app}^2$	$y_{part}(t) = \frac{F_{app} \cos(\omega_{app} t)}{M(\omega_{char} + \omega_{app})(\omega_{char} - \omega_{app})}$
Undamped, Frequency- Matched	$\eta = 0$ $\omega_{char}^2 = \frac{K_s}{M} = \omega_{app}^2$	$y_{part}(t) = \frac{F_{app}t\sin(\omega_{app}t)}{2M\omega_{app}}$
Damped	$\eta>0$	$y_{part}(t) = \frac{F_{app}\cos(\omega_{app}t + \phi_{lag})}{\sqrt{M^2(\omega_{char}^2 - \omega_{app}^2)^2 + \omega_{app}^2 \eta^2 l_o^2}}$ $\phi_{lag} = \tan^{-1}\left(\frac{\omega_{app}\eta l_o}{M(\omega_{char}^2 - \omega_{app}^2)}\right)$

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The phenomenon of resonance can be observed as the driving frequency approaches the characteristic frequency.

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Resonance and Near-Resonance Behavior

Solutions to $m\ddot{y} + \eta\dot{y} + ky = F_{app}\cos(\omega_{app}t)$ analyzed near the resonance condition $\omega_{app} \approx \omega_{char} \equiv \sqrt{k/m}$.

Kspring = Mωchar² Mathematica can solve the nonhomogeneous ODE with a forcing function at with an applied frequency: yGeneralSol = Simplify[y[t] /. DSolve[$My''[t] + \eta y'[t] + Kspringy[t] =$ Fapp Cos [ωapp t], y[t], t][[1]]] Consider the behavior of the general solution at time t=0. This will show that the homogeneous parts of the solution are needed to satisfy boundary conditions, even if the oscillator is initially at rest at zero displacement (i.e., $y(0) = \dot{y}(0) = 0$). Simplify[yGeneralSol /. t -> 0] Consider the particular case of anequilibrium at-rest oscillator vParticularSol = Simplify[y[t] /. DSolve[{My''[t] + $\eta y'[t] + Kspring y[t] =$ Fapp $Cos[\omega app t]$, y[0] == 0, y'[0] == 0}, y[t], t][[1]]] The resonant solution is the case: ωapp → D ResonantSolution = Simplify[yParticularSol /. ωapp → ωchar] ResonantSolutionSmallViscosity = Map[Simplify[PowerExpand[ExpToTrig[#]]] &, Normal[Series[ResonantSolution, $\{\eta, 0, 2\}$]]]

ResonantSolutionSmallViscosityDetuned =

PowerExpand [ExpToTrig[#]]] &,

Normal[Series[yParticularSol, $\{\omega app, \omega char, 1\}, \{\eta, 0, 2\}]]]$

Map[Simplify[

- 2: The general solution will include two arbitrary constants C[1] and C[2] in terms that derive from the homogeneous solution plus a part that derives from the heterogeneous (i.e., forced) part.
- 3: Examining the form of the general solution at t=0, it will be clear that the constants from the homogeneous part will be needed to satisfy arbitrary boundary conditions—most importantly, the constants will include terms that depend on the characteristic and applied frequencies.
- 4: Here DSolve will be used yParticularSolution to analyze the particular case of a forced (F(t) = $F_{app}\cos(\omega_{app}t)$) and damped harmonic oscillator initially at resting equilibrium (y(t=0)=1) and y'(t=0)=0).
- 5: The most interesting cases are the resonance and near resonance cases: Resonant Solution is obtained by setting the forcing frequency equal to the characteristic frequency.
- 6: To analyze the at-resonance case, the solution will be expanded to second order for small viscosity with Series. Some extra manipulation is required to display the results in a form that is straightforward to interpret. Here, Map will be used with a pure function to simplify each term produced by Series. First, the SeriesData object created by Series is transformed into a regular expression with Normal. The pure function will first transform any $\exp(x)$ into $\cosh(x) + \sinh(x)$, then any fractional powers will be cleaned up (e.g., $\sqrt{x^2 \to x}$) assuming real parameters; finally the individual terms will be simplified.
- 6: This illustrates how near resonance $\omega_{app} \approx \omega_{char}$ can be analyzed in the small viscosity limit. Here, Series first expands around $\eta = 0$ to second order and then around small $\delta \omega = \omega_{app} - \omega_{char}$.
- 7: Setting the viscosity to zero a priori is possible and returns the leading order behavior, but the asymptotic behavior for small parameters cannot be ascertained.

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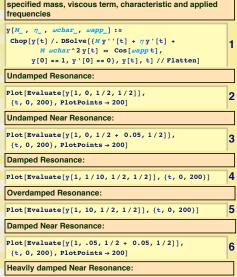
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Plot[Evaluate[y[1, 2.5, 1/2 + 0.05, 1/2]],

{t, 0, 200}, PlotPoints → 200]

Create a Mathematica function that returns the solution for

1: This function solves the heterogeneous damped harmonic oscillator ODE (where $F(t) = \cos(\omega_{app}t)$)

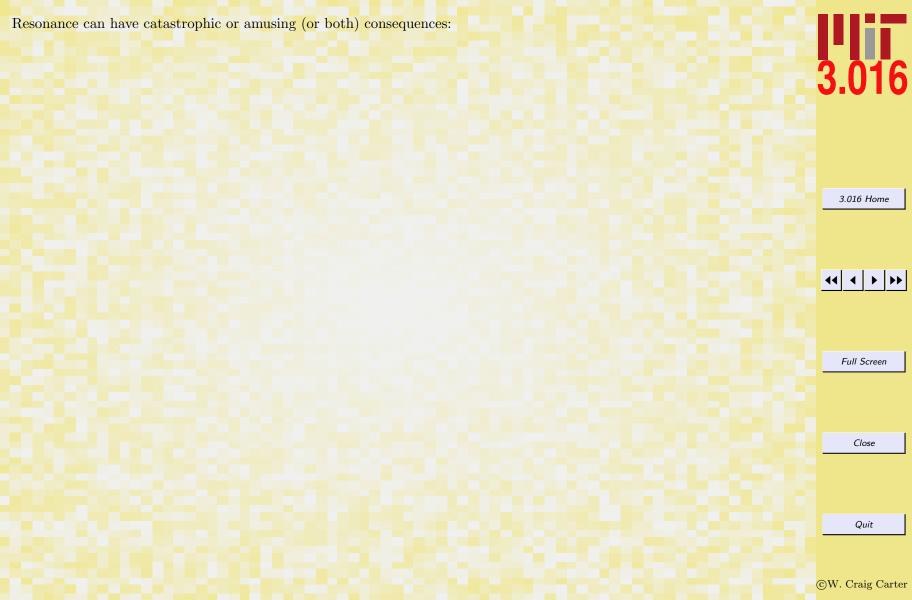
- for any input mass, damping coefficient, and spring constant M, η , $k = M\omega_{char}^2$. 2: Undamped resonance $\omega_{char} = \omega_{app} = 1/2$ should show linearly growing amplitude.
- 3: Near resonance will show a beat-phenomena because of "de-tuning."
- 4: Damped resonance will show that the amplitudes approaching to a finite asymptotic limit.
- 6: The beats will still be apparent for the damped near resonance condition, but the finite damping coefficient will prevent the amplitude from completely disappearing.

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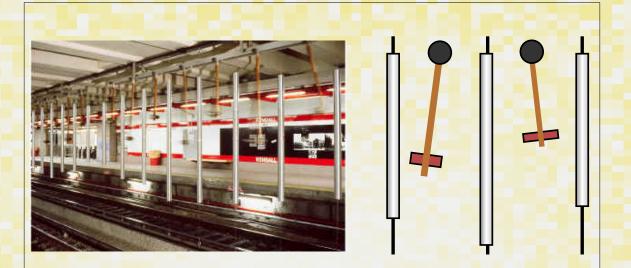


Figure 23-24: Picture and illustration of the bells at Kendall square. Many people shake the handles vigorously but with apparently no pleasant effect. The concept of resonance can be used to to operate the bells efficiently Perturb the handle slightly and observe the frequencies of the the pendulums—select one and wiggle the handle at the pendulum's characteristic frequency. The amplitude of that pendulum will increase and eventually strike the neighboring tubular bells.

From Cambridge Arts Council Website:

http://www.ci.cambridge.ma.us/~CAC/public_art_tour/map_11_kendall.html

A<mark>rt</mark>ist: Paul Matisse Title: The Kendall Band - Kepler, Pythagoras, Galileo Date: 1987

Materials: Aluminum, teak, steel

Handles located on the platforms allow passengers to play these mobile-like instruments, which are suspended in arches between the tracks, "Kepler" is an aluminum ring that will hum for five minutes after it is struck by the large teak hammer above it. "Pythagoras" consists of a 48-foot row of chimes made from heavy aluminum tubes interspersed with 14 teak hammers. "Galileo" is a large sheet of metal that rattles thunderously when one shakes the handle.



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Figure 23-25: Animation Available in individual lecture, deleted here because of filesize constraints. The Tacoma bridge disaster is perhaps one of the most well-knownfailures that resulted directly from resonance phenomena. It is believed that the wind blowing across the bridge caused the bridge to vibrate like a reed in a clarinet. (Images from Promotional Video Clip from *The Camera Shop 1007 Pacific Ave., Tacoma, Washington* Full video Available http://www.camerashoptacoma.com/)



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